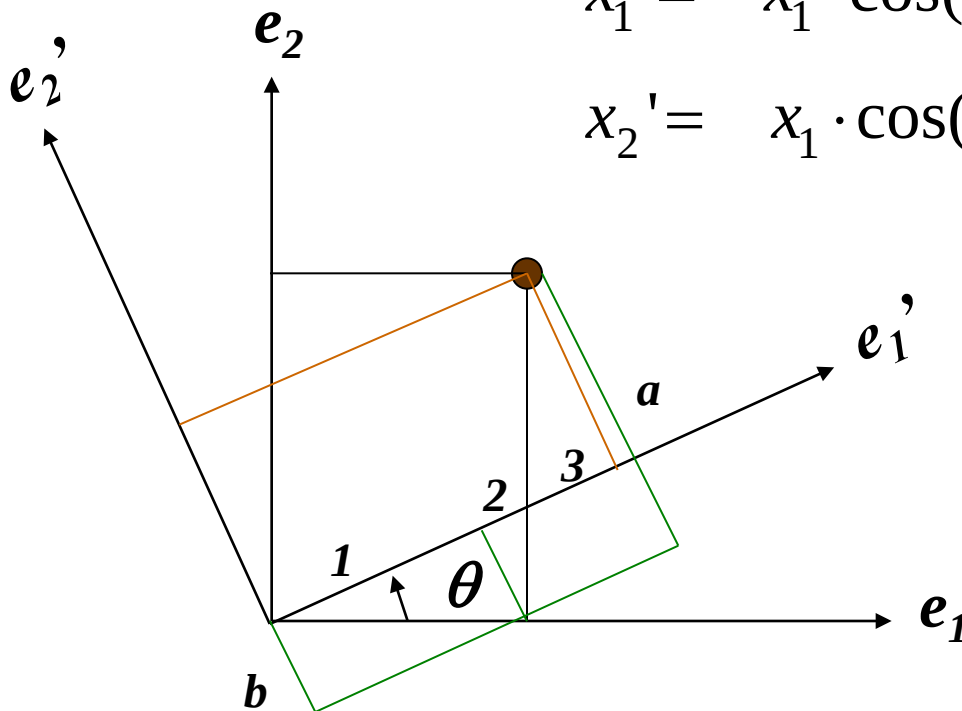


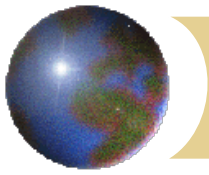
座標轉換

$$\begin{aligned} x_1' &= x_1 \cdot \cos \theta + x_2 \sin \theta \\ x_2' &= -x_1 \cdot \sin \theta + x_2 \cos \theta \end{aligned} \quad x_i' = \beta_{ij} \cdot x_j$$

$$\begin{aligned} x_1' &= x_1 \cdot \cos(e_1', e_1) + x_2 \cos(e_1', e_2) \\ x_2' &= x_1 \cdot \cos(e_2', e_1) + x_2 \cos(e_2', e_2) \end{aligned}$$



$$\begin{aligned} \beta_{ij} &= \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \\ &= \begin{bmatrix} \cos(\hat{e}_1', \hat{e}_1) & \cos(\hat{e}_1', \hat{e}_2) \\ \cos(\hat{e}_2', \hat{e}_1) & \cos(\hat{e}_2', \hat{e}_2) \end{bmatrix} \end{aligned}$$



座標轉換

$$x_1' = x_1 \cdot \cos(e_1', e_1) + x_2 \cos(e_1', e_2)$$

$$x_2' = x_1 \cdot \cos(e_2', e_1) + x_2 \cos(e_2', e_2)$$

$$x_i' = \beta_{ij} \cdot x_j \quad \beta_{ij} = \begin{bmatrix} \cos(\hat{e}_1', \hat{e}_1) & \cos(\hat{e}_1', \hat{e}_2) \\ \cos(\hat{e}_2', \hat{e}_1) & \cos(\hat{e}_2', \hat{e}_2) \end{bmatrix}$$

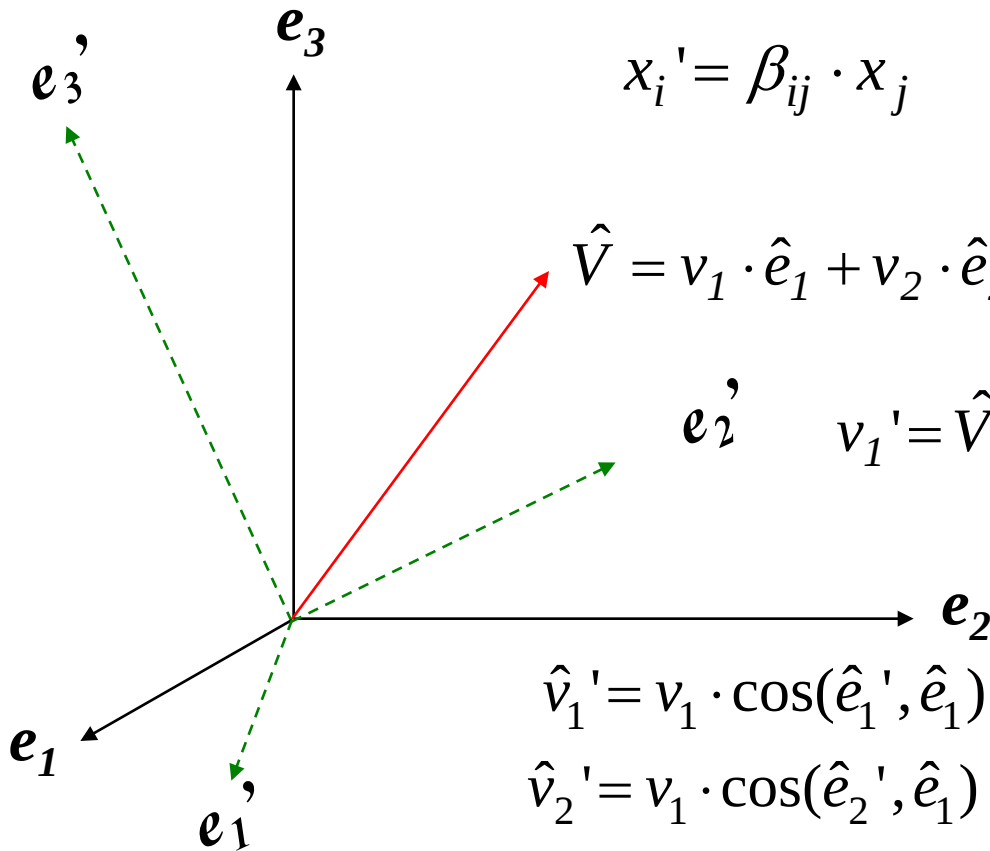
$$\hat{V} = v_1 \cdot \hat{e}_1 + v_2 \cdot \hat{e}_2 + v_3 \cdot \hat{e}_3 = v_1' \cdot \hat{e}_1' + v_2' \cdot \hat{e}_2' + v_3' \cdot \hat{e}_3'$$

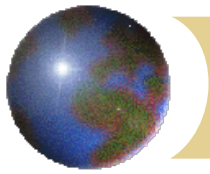
$$v_1' = \hat{V} \cdot \hat{e}_1'; \quad v_2' = \hat{V} \cdot \hat{e}_2'; \quad v_3' = \hat{V} \cdot \hat{e}_3'$$

$$\hat{v}_1' = v_1 \cdot \cos(\hat{e}_1', \hat{e}_1) + v_2 \cdot \cos(\hat{e}_1', \hat{e}_2) + v_3 \cdot \cos(\hat{e}_1', \hat{e}_3)$$

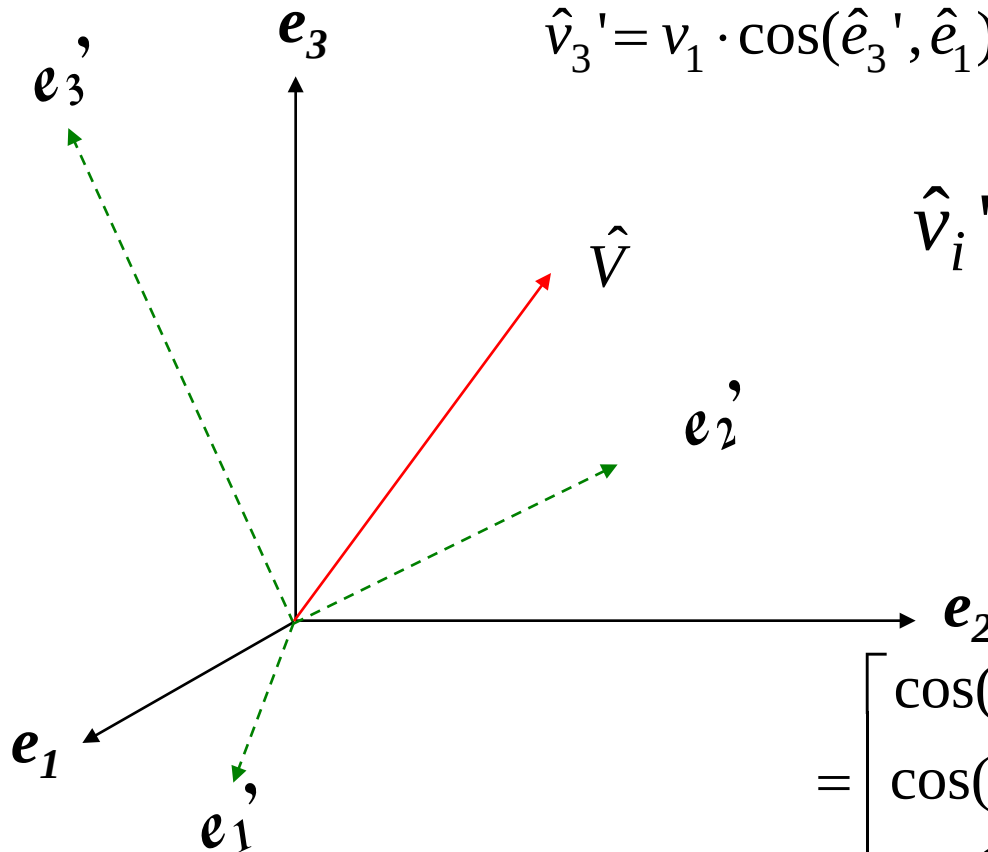
$$\hat{v}_2' = v_1 \cdot \cos(\hat{e}_2', \hat{e}_1) + v_2 \cdot \cos(\hat{e}_2', \hat{e}_2) + v_3 \cdot \cos(\hat{e}_2', \hat{e}_3)$$

$$\hat{v}_3' = v_1 \cdot \cos(\hat{e}_3', \hat{e}_1) + v_2 \cdot \cos(\hat{e}_3', \hat{e}_2) + v_3 \cdot \cos(\hat{e}_3', \hat{e}_3)$$





座標轉換



$$\hat{v}_1' = v_1 \cdot \cos(\hat{e}_1', \hat{e}_1) + v_2 \cdot \cos(\hat{e}_1', \hat{e}_2) + v_3 \cdot \cos(\hat{e}_1', \hat{e}_3)$$

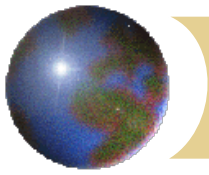
$$\hat{v}_2' = v_1 \cdot \cos(\hat{e}_2', \hat{e}_1) + v_2 \cdot \cos(\hat{e}_2', \hat{e}_2) + v_3 \cdot \cos(\hat{e}_2', \hat{e}_3)$$

$$\hat{v}_3' = v_1 \cdot \cos(\hat{e}_3', \hat{e}_1) + v_2 \cdot \cos(\hat{e}_3', \hat{e}_2) + v_3 \cdot \cos(\hat{e}_3', \hat{e}_3)$$

$$\hat{v}_i' = l_{ij} \cdot v_j \quad l_{ij} = \hat{e}_i' \cdot \hat{e}_j$$

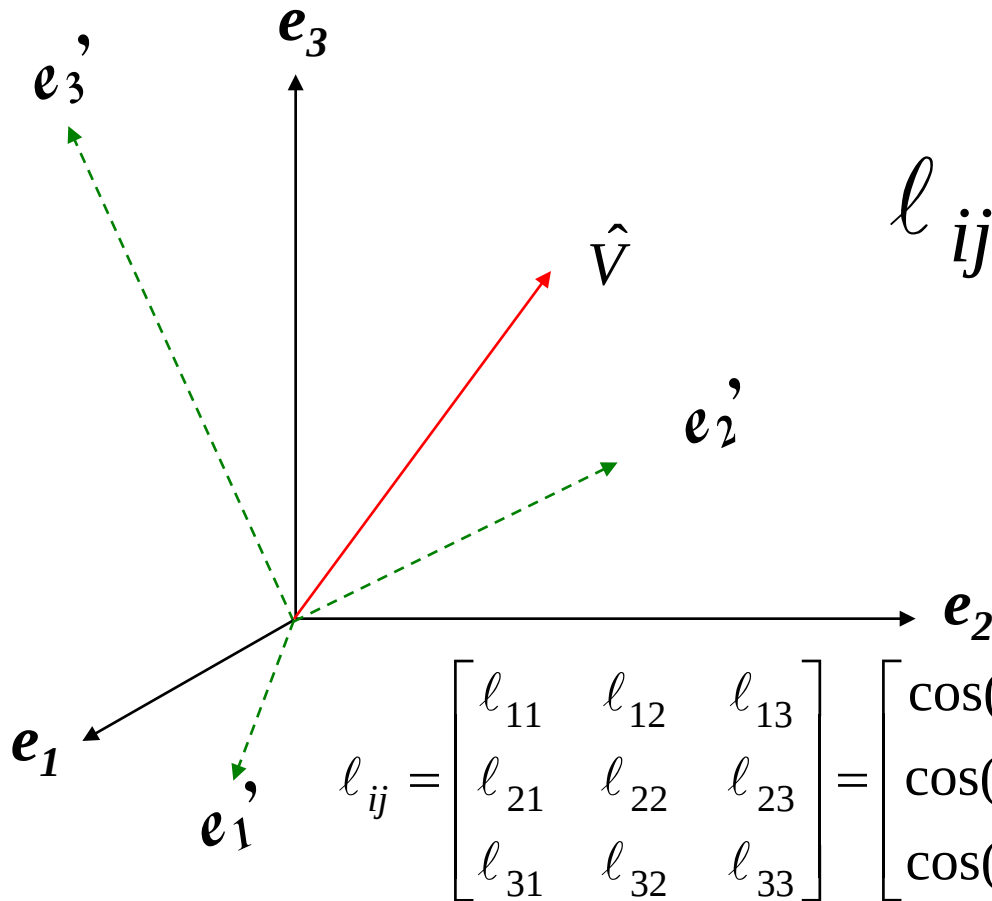
$$l_{ij} = \begin{bmatrix} l_{11} & l_{12} & l_{13} \\ l_{21} & l_{22} & l_{23} \\ l_{31} & l_{32} & l_{33} \end{bmatrix}$$

$$= \begin{bmatrix} \cos(\hat{e}_1', \hat{e}_1) & \cos(\hat{e}_1', \hat{e}_2) & \cos(\hat{e}_1', \hat{e}_3) \\ \cos(\hat{e}_2', \hat{e}_1) & \cos(\hat{e}_2', \hat{e}_2) & \cos(\hat{e}_2', \hat{e}_3) \\ \cos(\hat{e}_3', \hat{e}_1) & \cos(\hat{e}_3', \hat{e}_2) & \cos(\hat{e}_3', \hat{e}_3) \end{bmatrix}$$



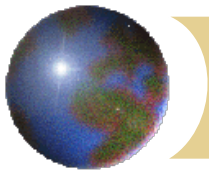
座標轉換

$$\hat{v}_i' = \ell_{ij} \cdot v_j$$



$$\ell_{ij} = \hat{\mathbf{e}}_i' \cdot \hat{\mathbf{e}}_j$$

方向餘弦



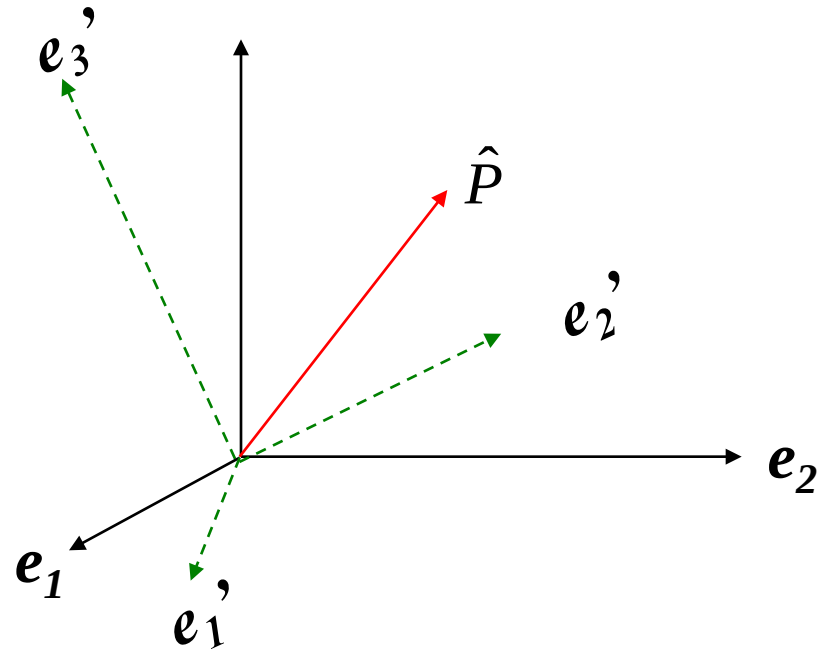
HW2

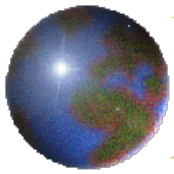
某一位移向量 $\hat{P}$ 於原座標系統為 $\hat{P} = u \cdot \hat{e}_1 + v \cdot \hat{e}_2 + w \cdot \hat{e}_3$ ($u = 3m; v = 3m; w = 3m$)
請問於旋轉後新座標系統此一位移向量 $\hat{P}'$ 為何？

$$\hat{e}_1' = 0.071 \cdot \hat{e}_1 + 0.816 \cdot \hat{e}_2 + 0.574 \cdot \hat{e}_3$$

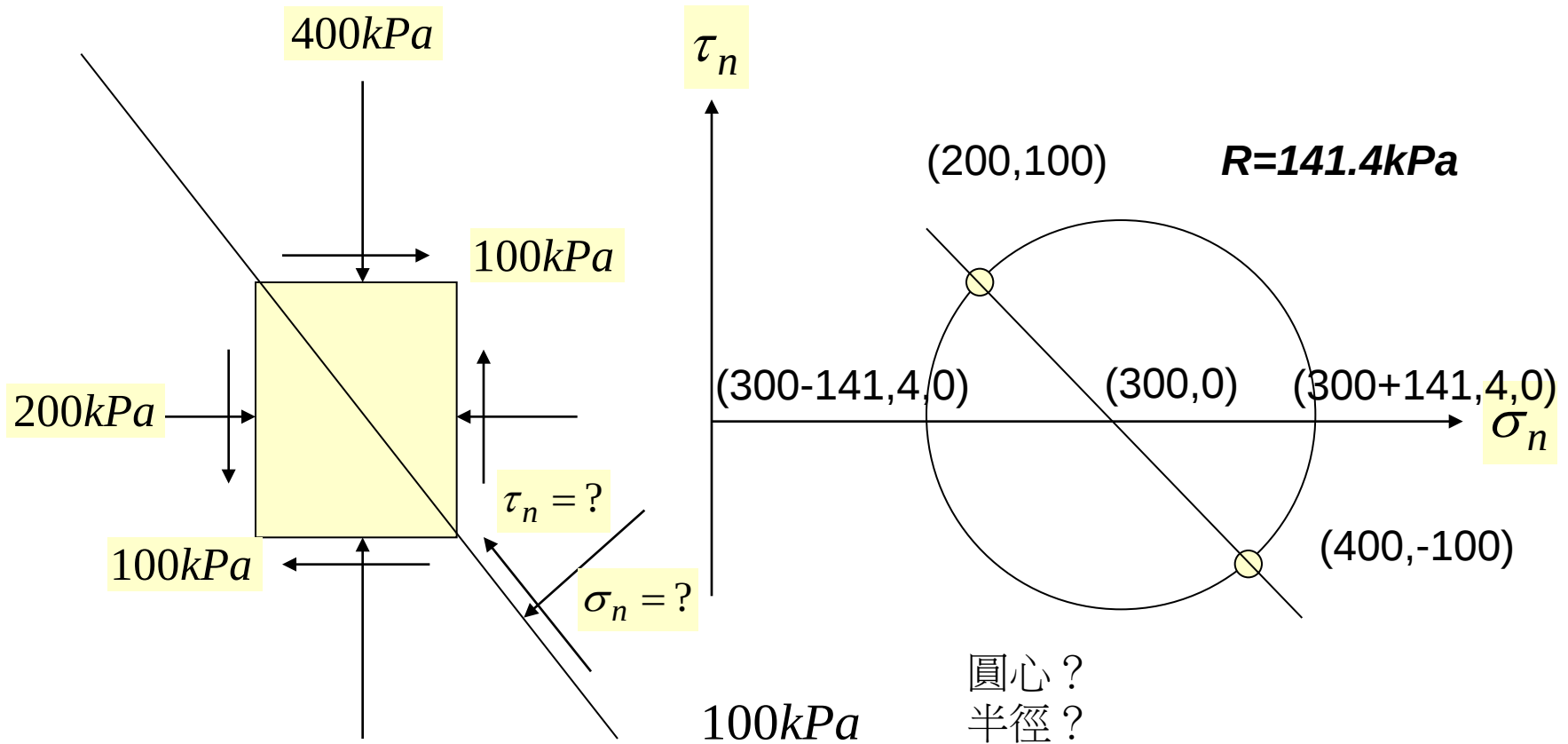
$$\hat{e}_2' = -0.584 \cdot \hat{e}_1 - 0.440 \cdot \hat{e}_2 + 0.682 \cdot \hat{e}_3$$

$$\hat{e}_3' = 0.808 \cdot \hat{e}_1 - 0.377 \cdot \hat{e}_2 + 0.454 \cdot \hat{e}_3$$



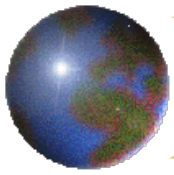


Construct a Mohr circle



主應力之定義為何?

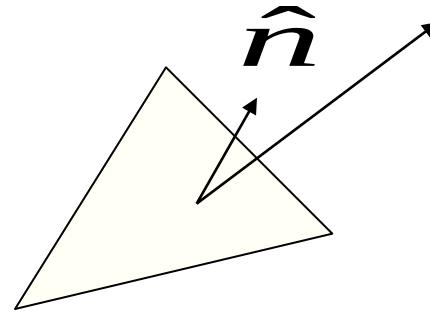
圓心?
半徑?
最大主應力?
最小主應力?
主應力方向?



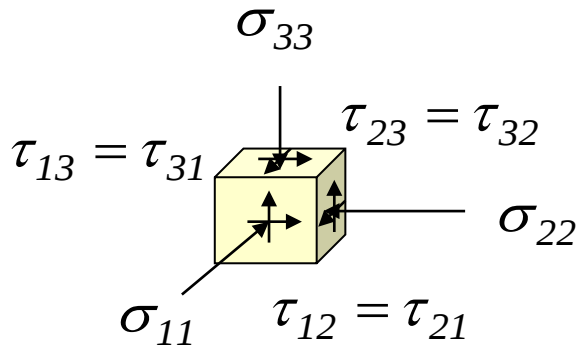
Three dimensional stress analysis

2.4 Principal stress and stress invariants

Principal stress and principal direction

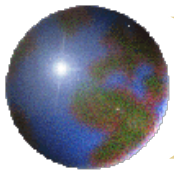


$$\hat{n} = \hat{n}_1 + \hat{n}_2 + \hat{n}_3$$



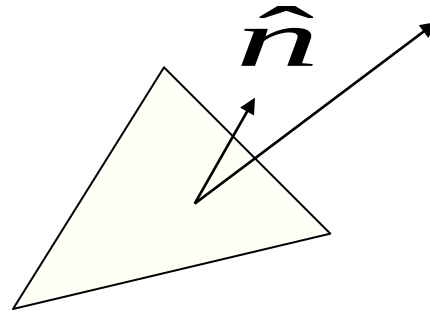
$$\hat{n}_i T_i = \sigma_{ji} \cdot n_j = \sigma_{ij} \cdot n_j$$

剪應力為 0 之平面為主應力面
該面上作用之正向應力為主應力

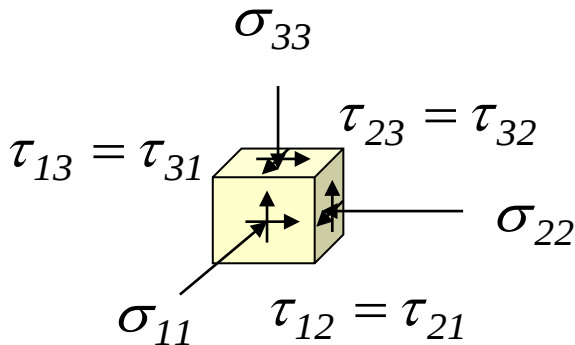


Three dimensional stress analysis

Principal stress and principal direction



$$\hat{n} = \hat{n}_1 + \hat{n}_2 + \hat{n}_3$$



$$\hat{n}_i T_i = \hat{\sigma}_n = \sigma \cdot n_i$$

$$\tau_n = 0$$

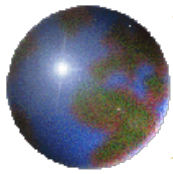
Principal stress

$$\hat{\sigma}_n$$

principal direction

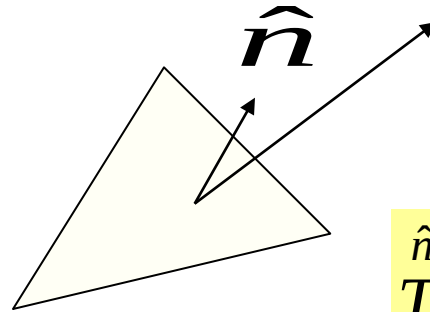
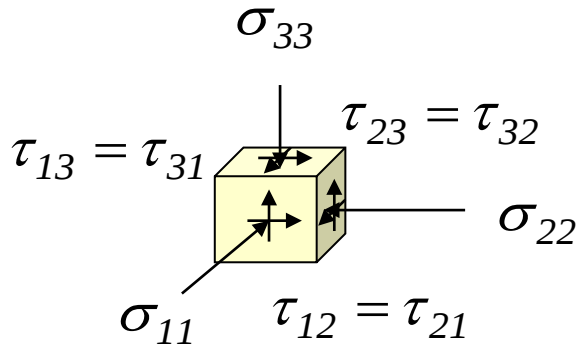
$$\hat{n}$$

剪應力為 0 之平面為主應力面
該面上作用之正向應力為主應力



Three dimensional stress analysis

Principal stress and principal direction



$$\hat{n} T = \overset{1}{T} \cdot n_1 + \overset{2}{T} \cdot n_2 + \overset{3}{T} \cdot n_3$$

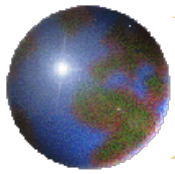
$$\hat{n} T_i = \hat{\sigma}_n = \sigma \cdot n_i \quad \tau_n = 0$$

$$\hat{n} T_i = \sigma \cdot n_i$$

$$\hat{n} T_i = \sigma_{ij} \cdot n_j$$

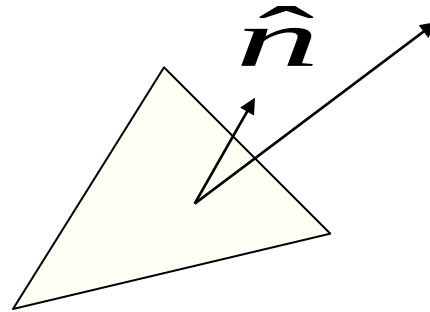
$$\sigma_{ij} \cdot n_j = \sigma \cdot n_i$$

剪應力為 0 之平面為主應力面
該面上作用之正向應力為主應力



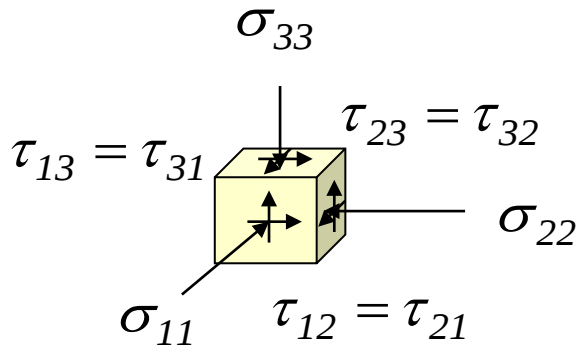
Three dimensional stress analysis

Principal stress and principal direction



$$\hat{n} = \hat{n}_1 + \hat{n}_2 + \hat{n}_3$$

$$\sigma_{ij} \cdot n_j = \sigma \cdot n_i$$

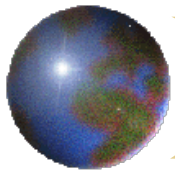


$$\sigma_{11} \cdot n_1 + \sigma_{12} \cdot n_2 + \sigma_{13} \cdot n_3 = \sigma \cdot n_1$$

$$\sigma_{21} \cdot n_1 + \sigma_{22} \cdot n_2 + \sigma_{23} \cdot n_3 = \sigma \cdot n_2$$

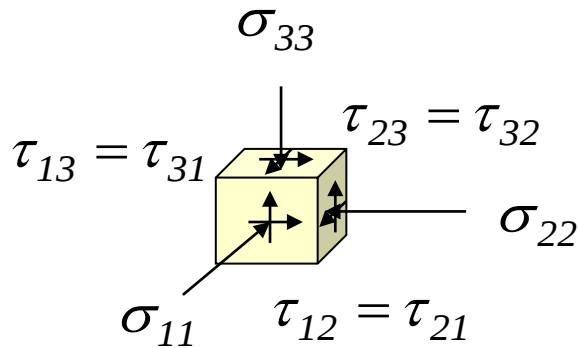
$$\sigma_{31} \cdot n_1 + \sigma_{32} \cdot n_2 + \sigma_{33} \cdot n_3 = \sigma \cdot n_3$$

剪應力為0之平面為主應力面
該面上作用之正向應力為主應力



Three dimensional stress analysis

Principal stress and principal direction



$$\hat{n} \quad T = T \cdot n_1 + T \cdot n_2 + T \cdot n_3$$

$$\sigma_{11} \cdot n_1 + \sigma_{12} \cdot n_2 + \sigma_{13} \cdot n_3 = \sigma \cdot n_1$$

$$\sigma_{21} \cdot n_1 + \sigma_{22} \cdot n_2 + \sigma_{23} \cdot n_3 = \sigma \cdot n_2$$

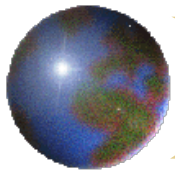
$$\sigma_{31} \cdot n_1 + \sigma_{32} \cdot n_2 + \sigma_{33} \cdot n_3 = \sigma \cdot n_3$$

剪應力為 0 之平面為主應力面
該面上作用之正向應力為主應力

$$\begin{bmatrix} \sigma_{11} - \sigma & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \sigma & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - \sigma \end{bmatrix} \cdot \begin{bmatrix} n_1 \\ n_2 \\ n_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

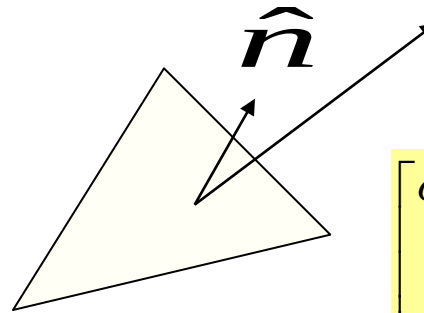
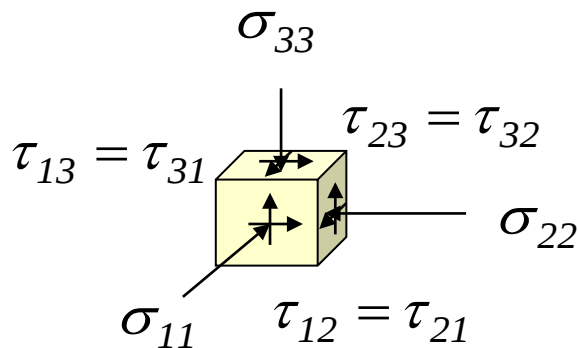
For non-trivial solution of n

$$\begin{vmatrix} \sigma_{11} - \sigma & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \sigma & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - \sigma \end{vmatrix} = 0$$



Three dimensional stress analysis

Principal stress and principal direction



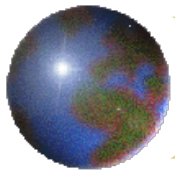
$$\hat{T} = T \cdot n_1 + T \cdot n_2 + T \cdot n_3$$

$$\begin{bmatrix} \sigma_{11} - \sigma & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \sigma & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - \sigma \end{bmatrix} \cdot \begin{bmatrix} n_1 \\ n_2 \\ n_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

剪應力為 0 之平面為主應力面
該面上作用之正向應力為主應力

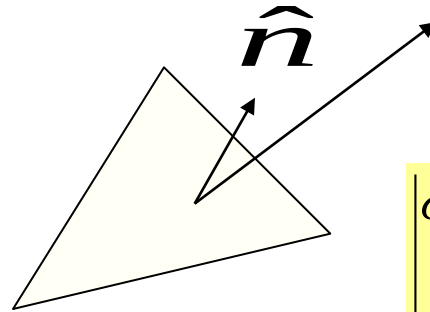
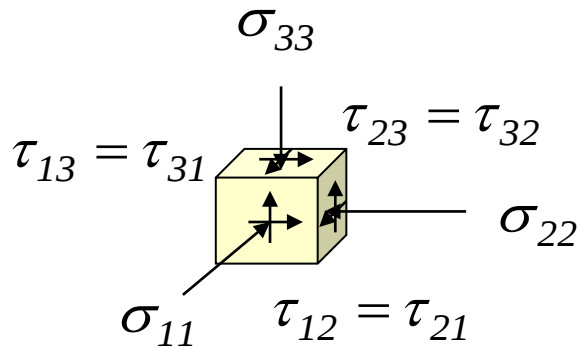
$$\begin{vmatrix} \sigma_{11} - \sigma & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \sigma & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - \sigma \end{vmatrix} = 0$$

3 solutions of stress represent 3 principal stresses
Correspond orthogonal directions are principal directions



Three dimensional stress analysis

Principal stress and principal direction



$$\hat{n} = \hat{n}_1 + \hat{n}_2 + \hat{n}_3$$

$$T = T \cdot n_1 + T \cdot n_2 + T \cdot n_3$$

$$\begin{vmatrix} \sigma_{11} - \sigma & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \sigma & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - \sigma \end{vmatrix} = 0$$

剪應力為 0 之平面為主應力面
該面上作用之正向應力為主應力

$$\sigma^3 - I_1 \cdot \sigma^2 + I_2 \cdot \sigma - I_3 = 0$$

3 solutions of stress represent 3 principal stresses

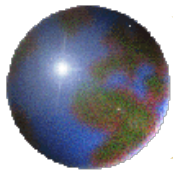
$$\sigma_1, \sigma_2, \sigma_3$$

Correspond orthogonal directions
are principal directions

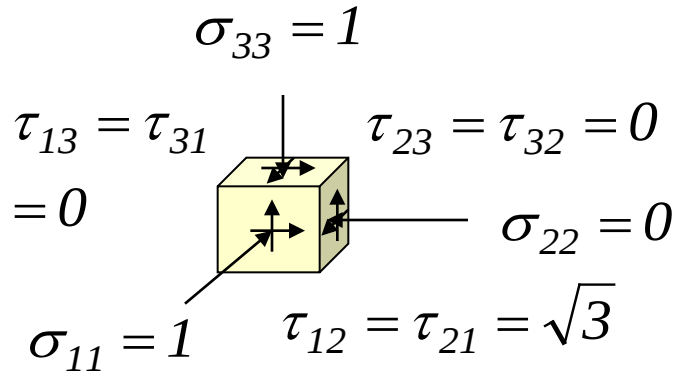
$$\sigma = \sigma_1$$

$$n_1^{(1)}, n_2^{(1)}, n_3^{(1)}$$

$$\begin{bmatrix} \sigma_{11} - \sigma_1 & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \sigma_1 & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - \sigma_1 \end{bmatrix} \cdot \begin{bmatrix} n_1 \\ n_2 \\ n_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$



Three dimensional stress analysis



$$\sigma_{ij} = \begin{bmatrix} 1 & \sqrt{3} & 0 \\ \sqrt{3} & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Principal stresses =?
Principal directions =?

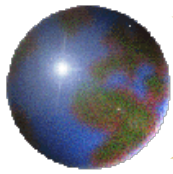
$$\begin{vmatrix} \sigma_{11} - \sigma & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \sigma & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - \sigma \end{vmatrix} = 0$$

$$\begin{vmatrix} 1 - \sigma & \sqrt{3} & 0 \\ \sqrt{3} & -\sigma & 0 \\ 0 & 0 & 1 - \sigma \end{vmatrix} = 0$$

$$(\sigma - 1)(\sigma^2 - \sigma - 3) = 0$$

3 solutions of stress represent 3 principal stresses

$$\sigma_1 = \frac{1 + \sqrt{13}}{2}, \sigma_2 = 1, \sigma_3 = \frac{1 - \sqrt{13}}{2}$$



Three dimensional stress analysis

$$\sigma_{33} = 1$$

$$\begin{aligned} \tau_{13} &= \tau_{31} = 0 \\ \tau_{23} &= \tau_{32} = 0 \\ \sigma_{22} &= 0 \\ \sigma_{11} &= 1 \\ \tau_{12} &= \tau_{21} = \sqrt{3} \end{aligned}$$

$$\sigma_{ij} = \begin{bmatrix} 1 & \sqrt{3} & 0 \\ \sqrt{3} & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Principal stresses =?
Principal directions =?

$$(\sigma - 1)(\sigma^2 - \sigma - 3) = 0$$

$$\sigma_1 = \frac{1 + \sqrt{13}}{2}, \sigma_2 = 1, \sigma_3 = \frac{1 - \sqrt{13}}{2}$$

$$\sigma = \sigma_2$$

Correspond orthogonal directions
are *principal directions*

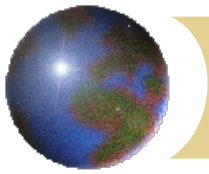
$$\begin{bmatrix} \sigma_{11} - \sigma_2 & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \sigma_2 & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - \sigma_2 \end{bmatrix} \cdot \begin{bmatrix} n_1 \\ n_2 \\ n_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} 1 - 1 & \sqrt{3} & 0 \\ \sqrt{3} & 0 - 1 & 0 \\ 0 & 0 & 1 - 1 \end{bmatrix} \cdot \begin{bmatrix} n_1^{(2)} \\ n_2^{(2)} \\ n_3^{(2)} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$(n_1^{(2)}, n_2^{(2)}, n_3^{(2)}) = (0, 0, 1)$$

$$n_1^2 + n_2^2 + n_3^2 = 1$$

$$(n_1^{(1)}, n_2^{(1)}, n_3^{(1)}) = (0.8, 0.6, 0); (n_1^{(3)}, n_2^{(3)}, n_3^{(3)}) = (0.6, -0.8, 0)$$



HW3

Given a stress tensor $\sigma_{ij} = \begin{pmatrix} 1 & 0 & -1 \\ 0 & -1 & 0 \\ -1 & 0 & 1 \end{pmatrix}$ (GPa) ,

Please find : (1) three principal stresses ; (2) three principal directions ◦

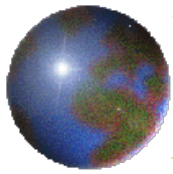
Given a fault plane N-S strike 、 dip angle 90° (vertical plane)

Please find : (1) Surface traction $\hat{T}_i$; (2) normal stress ; (3) shear stress ◦

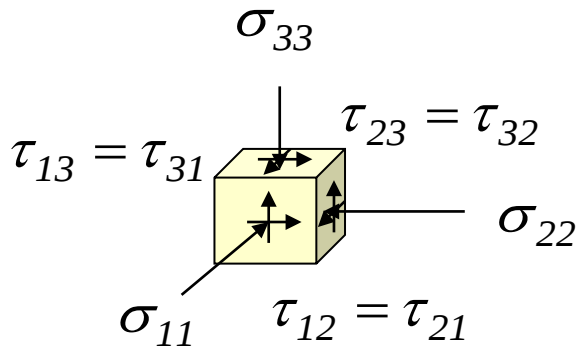
If the stress state of the fault was measured just before the fault slip (shear stress=shear strength), please determine the friction coefficient of the fault ?

Hint: direction 1 in Eastern-ward, direction 2 in Northern-ward, direction 3 in up-ward, friction coefficient

$$\mu = \tau_n / \sigma_n$$



The invariants of stress tensor



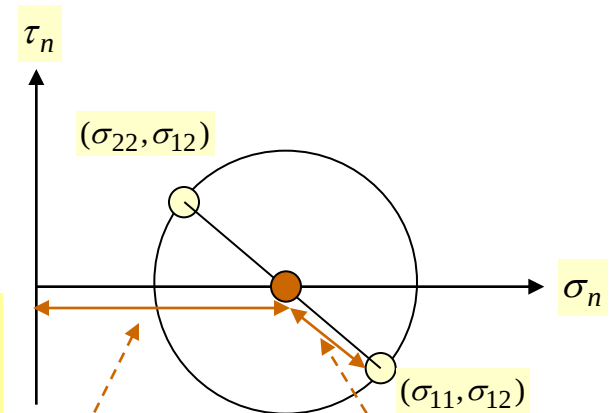
$$\begin{vmatrix} \sigma_{11} - \sigma & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \sigma & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - \sigma \end{vmatrix} = 0$$

$$\sigma^3 - I_1 \cdot \sigma^2 + I_2 \cdot \sigma - I_3 = 0$$

$$I_1 = \sigma_{11} + \sigma_{22} + \sigma_{33}$$

$$I_2 = \begin{vmatrix} \sigma_{22} & \sigma_{23} \\ \sigma_{32} & \sigma_{33} \end{vmatrix} + \begin{vmatrix} \sigma_{11} & \sigma_{13} \\ \sigma_{31} & \sigma_{33} \end{vmatrix} + \begin{vmatrix} \sigma_{11} & \sigma_{12} \\ \sigma_{21} & \sigma_{22} \end{vmatrix}$$

$$I_3 = \begin{vmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{vmatrix}$$

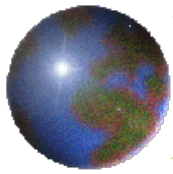


For two dimensional

$$\sigma^2 - (\sigma_{11} + \sigma_{22}) \cdot \sigma + (\sigma_{11} \cdot \sigma_{22} - \sigma_{12}^2) = 0$$

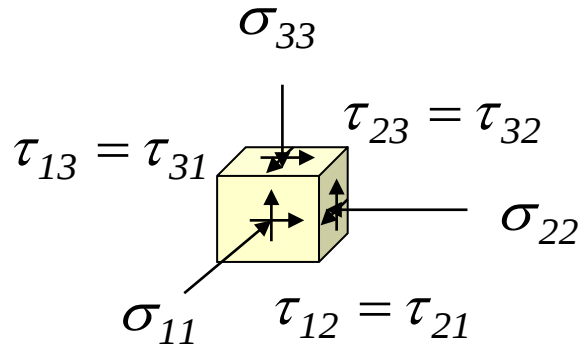
$$2 \times \left(\frac{\sigma_{11} + \sigma_{22}}{2} \right)$$

$$\left(\frac{\sigma_{11} + \sigma_{22}}{2} \right)^2 - \left[\left(\frac{\sigma_{11} - \sigma_{22}}{2} \right)^2 + \sigma_{12}^2 \right]$$



The invariants of stress tensor

$$\sigma^3 - I_1 \cdot \sigma^2 + I_2 \cdot \sigma - I_3 = 0$$



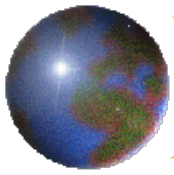
$$\sigma_{ij} = \begin{bmatrix} 1 & \sqrt{3} & 0 \\ \sqrt{3} & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\sigma_{ij} = \begin{bmatrix} \frac{1+\sqrt{13}}{2} & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & \frac{1-\sqrt{13}}{2} \end{bmatrix}$$

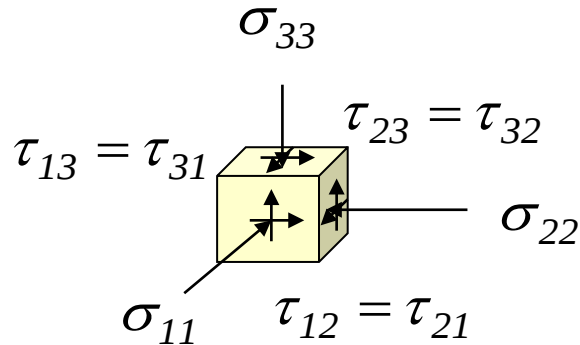
$$I_1 = \sigma_{11} + \sigma_{22} + \sigma_{33} = 2$$

$$I_2 = \begin{vmatrix} \sigma_{22} & \sigma_{23} \\ \sigma_{32} & \sigma_{33} \end{vmatrix} + \begin{vmatrix} \sigma_{11} & \sigma_{13} \\ \sigma_{31} & \sigma_{33} \end{vmatrix} + \begin{vmatrix} \sigma_{11} & \sigma_{12} \\ \sigma_{21} & \sigma_{22} \end{vmatrix} = -2$$

$$I_3 = \begin{vmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{vmatrix} = -3$$



The deviator stress



$$\sigma_{ij}^d = \sigma_{ij} - \frac{I_1}{3} \delta_{ij}$$

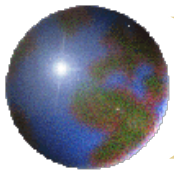
$$\sigma_{ij}^d = \begin{bmatrix} \sigma_{xx} - \sigma_m & \sigma_{xy} & \sigma_{xz} \\ \sigma_{xy} & \sigma_{yy} - \sigma_m & \sigma_{yz} \\ \sigma_{xz} & \sigma_{yz} & \sigma_{zz} - \sigma_m \end{bmatrix}$$

Principal deviator stresses

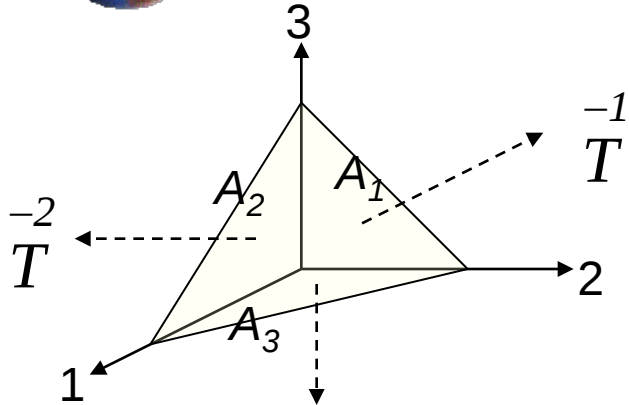
$$S_1 = \sigma_1 - \frac{I_1}{3},$$

$$S_2 = \sigma_2 - \frac{I_1}{3},$$

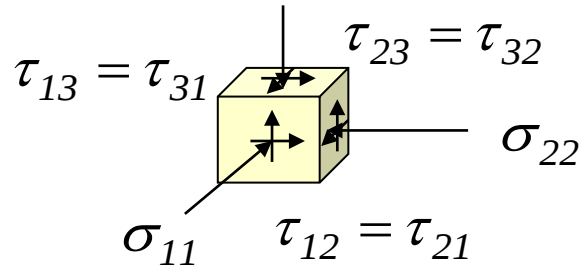
$$S_3 = \sigma_3 - \frac{I_1}{3},$$



Stress transformation



σ_{33}



$$n_l' = \ell_{lj} \cdot n_j$$

$$\begin{aligned} \ell_{lk} \cdot n_l' &= \ell_{lk} \cdot \ell_{lj} \cdot n_j \\ &= e_l' \cdot e_l' \cdot e_k \cdot e_j \cdot n_j \\ &= 1 \cdot \delta_{kj} \cdot n_j = n_k \end{aligned}$$

$$\hat{n} \cdot \hat{T} = \hat{T} \cdot n_1 + \hat{T} \cdot n_2 + \hat{T} \cdot n_3$$

$$\hat{T}_i = \sigma_{ji} \cdot n_j = \sigma_{ij} \cdot n_j$$

In matrix form

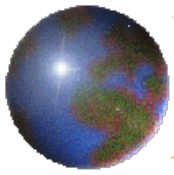
$$\begin{bmatrix} \hat{T}_1 \\ \hat{T}_2 \\ \hat{T}_3 \end{bmatrix} = \begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix} \cdot \begin{bmatrix} n_1 \\ n_2 \\ n_3 \end{bmatrix}$$

$$\hat{T}_i = \sigma_{ji} \cdot n_j = \sigma_{ij} \cdot n_j$$

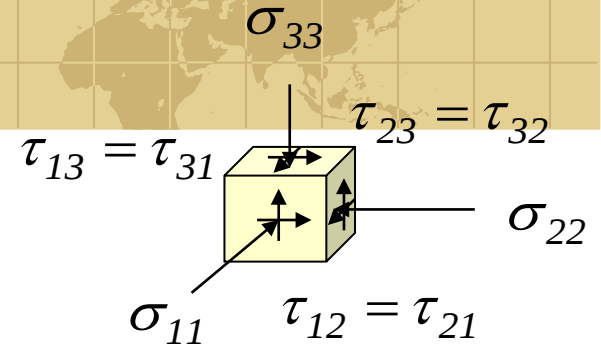
$$\hat{T}_i' = \ell_{ij} \cdot \hat{T}_j = \ell_{ij} \cdot \sigma_{jk} \cdot n_k = \ell_{ij} \cdot \sigma_{jk} \cdot \ell_{lk} \cdot n_l'$$

$$\hat{T}_i' = \sigma_{il}' \cdot n_l'$$

$$\therefore \sigma_{il}' = \ell_{ij} \cdot \sigma_{jk} \cdot \ell_{lk}$$



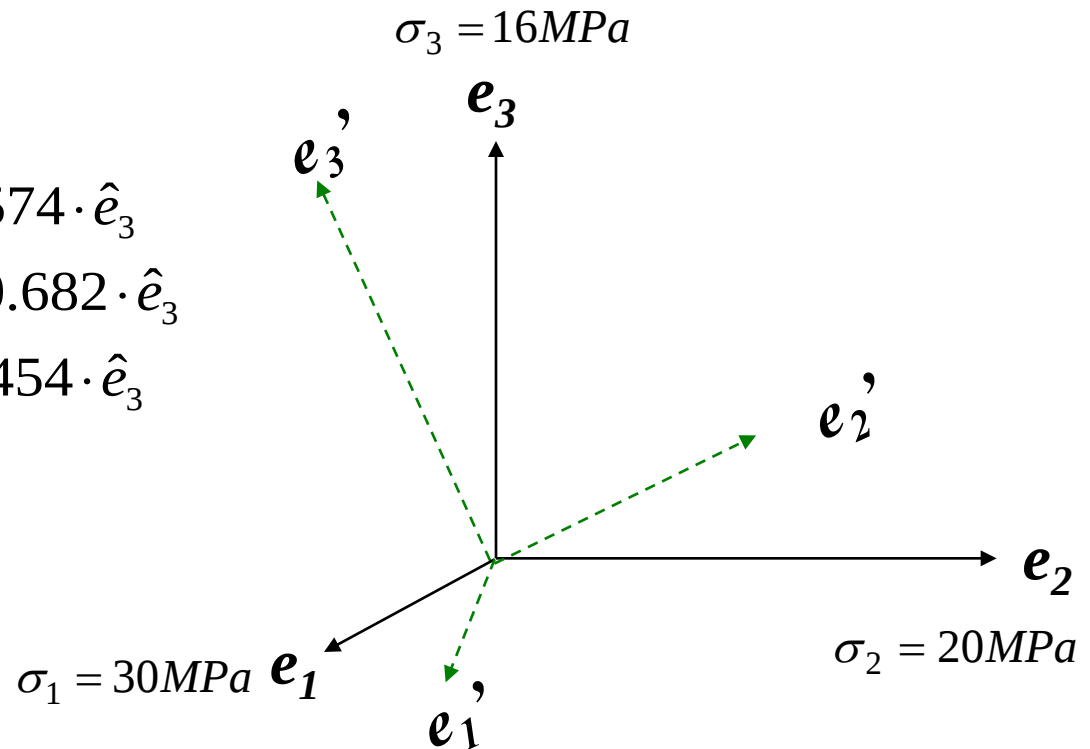
HW4

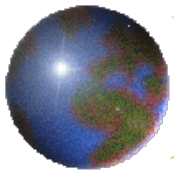


Please find the stress tensor in coordinate system $e_1'-e_2'-e_3'$

$$\begin{aligned}\hat{e}_1' &= 0.071 \cdot \hat{e}_1 + 0.816 \cdot \hat{e}_2 + 0.574 \cdot \hat{e}_3 \\ \hat{e}_2' &= -0.584 \cdot \hat{e}_1 - 0.440 \cdot \hat{e}_2 + 0.682 \cdot \hat{e}_3 \\ \hat{e}_3' &= 0.808 \cdot \hat{e}_1 - 0.377 \cdot \hat{e}_2 + 0.454 \cdot \hat{e}_3\end{aligned}$$

Please read section 2.3





大域座標下 $\sigma_{pq} = ?$

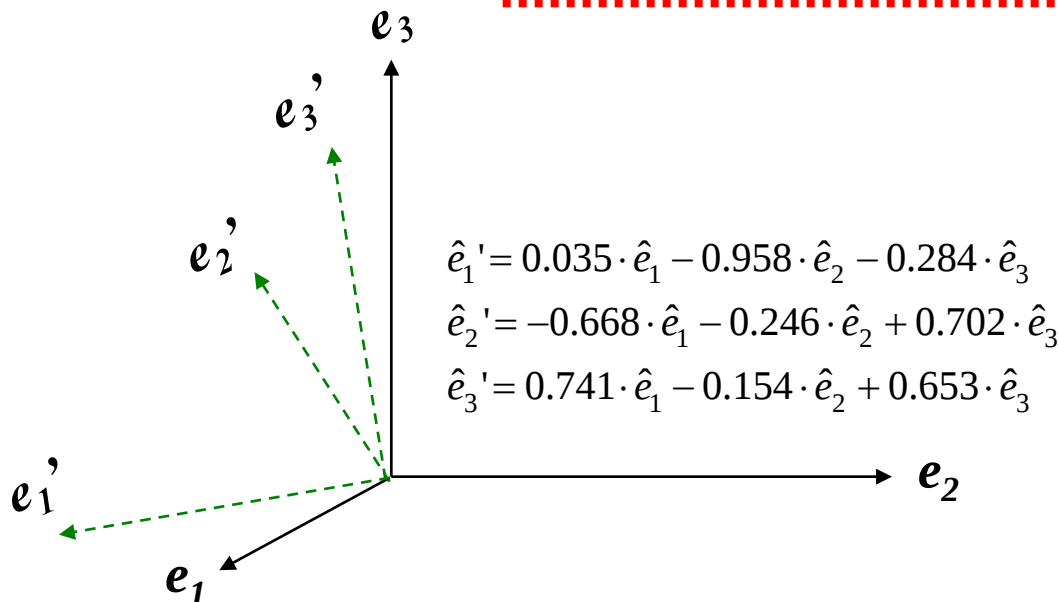
$$\sigma_{jk}' = \begin{bmatrix} 36.6 & 0 & 0 \\ 0 & 16 & 0 \\ 0 & 0 & 12.3 \end{bmatrix} (MPa)$$

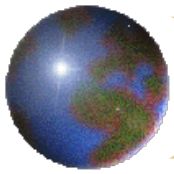
$$\ell_{ij} = \hat{e}_i' \cdot \hat{e}_j$$

$$\sigma_{il}' = \ell_{ij} \cdot \sigma_{jk} \cdot \ell_{lk}$$

$$\therefore \ell_{ip} \cdot \sigma_{il}' \cdot \ell_{lq} = \ell_{ip} \cdot \ell_{ij} \cdot \sigma_{jk} \cdot \ell_{lk} \cdot \ell_{lq} = \delta_{pj} \cdot \sigma_{jk} \cdot \delta_{kq} = \sigma_{pq}$$

$$\therefore \sigma_{pq} = \ell_{ip} \cdot \sigma_{il}' \cdot \ell_{lq} \quad \text{or} \quad \sigma_{il} = \ell_{ji} \cdot \sigma_{jk}' \cdot \ell_{kl}$$





Stress transformation

$$\begin{aligned}\hat{n} \\ T_i &= \sigma_{ji} \cdot n_j = \sigma_{ij} \cdot n_j \\ \hat{n} \\ T_i' &= \ell_{ij} \cdot \hat{T}_j = \ell_{ij} \cdot \sigma_{jk} \cdot n_k \\ \hat{n} \\ T_i' &= \sigma_{il}' \cdot n_l' = \sigma_{il}' \cdot \ell_{lk} \cdot n_k \\ \therefore \sigma_{il}' \cdot \ell_{lk} &= \ell_{ij} \cdot \sigma_{jk}\end{aligned}$$

In matrix form

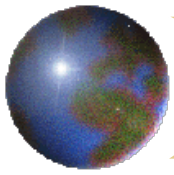
$$\begin{aligned}n_l' &= \ell_{lj} \cdot n_j \\ \ell_{lk} \cdot n_l' &= \ell_{lk} \cdot \ell_{lj} \cdot n_j \\ &= e_l' \cdot e_l' \cdot e_k \cdot e_j \cdot n_j \\ &= 1 \cdot \delta_{kj} \cdot n_j = n_k\end{aligned}$$

$$\begin{bmatrix} \sigma'_{11} & \sigma'_{12} & \sigma'_{13} \\ \sigma'_{21} & \sigma'_{22} & \sigma'_{23} \\ \sigma'_{31} & \sigma'_{32} & \sigma'_{33} \end{bmatrix} \cdot \begin{bmatrix} \ell_{11} & \ell_{12} & \ell_{13} \\ \ell_{21} & \ell_{22} & \ell_{23} \\ \ell_{31} & \ell_{32} & \ell_{33} \end{bmatrix} = \begin{bmatrix} \ell_{11} & \ell_{12} & \ell_{13} \\ \ell_{21} & \ell_{22} & \ell_{23} \\ \ell_{31} & \ell_{32} & \ell_{33} \end{bmatrix} \cdot \begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix}$$

$$\longrightarrow \begin{bmatrix} \sigma'_{11} & \sigma'_{12} & \sigma'_{13} \\ \sigma'_{21} & \sigma'_{22} & \sigma'_{23} \\ \sigma'_{31} & \sigma'_{32} & \sigma'_{33} \end{bmatrix} = \begin{bmatrix} \ell_{11} & \ell_{12} & \ell_{13} \\ \ell_{21} & \ell_{22} & \ell_{23} \\ \ell_{31} & \ell_{32} & \ell_{33} \end{bmatrix} \cdot \begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix} \cdot \begin{bmatrix} \ell_{11} & \ell_{12} & \ell_{13} \\ \ell_{21} & \ell_{22} & \ell_{23} \\ \ell_{31} & \ell_{32} & \ell_{33} \end{bmatrix}^T \quad \sigma_{il}' = \ell_{ij} \cdot \sigma_{jk} \cdot \ell_{lk}$$

$$\sigma_{il} = \ell_{ji} \cdot \sigma_{jk}' \cdot \ell_{kl} \quad \text{OR}$$

$$\begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix} = \begin{bmatrix} \ell_{11} & \ell_{12} & \ell_{13} \\ \ell_{21} & \ell_{22} & \ell_{23} \\ \ell_{31} & \ell_{32} & \ell_{33} \end{bmatrix}^T \cdot \begin{bmatrix} \sigma'_{11} & \sigma'_{12} & \sigma'_{13} \\ \sigma'_{21} & \sigma'_{22} & \sigma'_{23} \\ \sigma'_{31} & \sigma'_{32} & \sigma'_{33} \end{bmatrix} \cdot \begin{bmatrix} \ell_{11} & \ell_{12} & \ell_{13} \\ \ell_{21} & \ell_{22} & \ell_{23} \\ \ell_{31} & \ell_{32} & \ell_{33} \end{bmatrix}$$



Strength

- ⊕ A stress state that the materials cannot sustain
- ⊕ Failure

